5 QUALITY ASSURANCE PROCEDURES

Random Numbers

Design Mix Formula

Lot/Sublot -- QC/QA HMA and SMA

Acceptance Samples

Adjustment Period -- QC/QA HMA and SMA

Mixture Acceptance

QC/QA HMA HMA SMA

Pay Factors -- QC/QA HMA

Mixture Density

Mix Appeal -- QC/QA HMA

Adjustment Quantity -- QC/QA HMA

Adjustment Quantity -- SMA

Mixture Adjustment Factor

CHAPTER FIVE: QUALITY ASSURANCE PROCEDURES

The acceptance criteria for QC/QA HMA set out in the Quality Assurance Specifications are based on binder content, air voids @ N_{des} , VMA @ N_{des} , density and smoothness. The Specifications establish controls for temperature of the mixture, testing of aggregates for quality, and testing of binder. The acceptance criteria for HMA mixtures are based on binder content and air voids. The acceptance criteria for SMA mixtures are binder content and gradation.

This section includes the procedures for obtaining acceptance samples, minimum requirements for mixture properties in accordance with Sections **401** (QC/QA HMA), **402** (HMA), and **410** (SMA), and the procedures for determining pay factors.

RANDOM NUMBERS

Sampling for mixture tests is done on a random basis using **ITM 802**. A table of Random Numbers, as shown in Figure 5-1, is used to determine the random quantity or random location. The numbers occur in this table without aim or reason and are in no particular sequence. Therefore, samples obtained by the use of this table are truly random or chance, and eliminate any bias in obtaining samples.

To use the random number table to determine the random ton to sample, select without looking one block in the table. After selecting the block, the top left number in the block is the first random number used. This number is the beginning number. Proceed down the column for additional numbers and proceed to the top of the next column on the right when the bottom of the column is reached. When the bottom of the last column on the right is reached, proceed to the top of the column at the left. If all numbers in the table are used, select a new starting number and proceed in the same manner.

To use this table to determine the location of the pavement sample, again select a block in the table and start with the top left number. This number is used to determine the test site station. The adjacent number within the block is used to determine the transverse distance to the random site. Proceed down by pairs until the bottom numbers are reached and proceed to the adjacent top block to the right, if available. When the bottom pair of numbers on the right are reached, proceed to the top block on the left in the table.

0.576	0.730	0.430	0.754	0.271	0.870	0.732	0.721	0.998	0.239
0.892	0.948	0.858	0.025	0.935	0.114	0.153	0.508	0.749	0.291
0.669	0.726	0.501	0.402	0.231	0.505	0.009	0.420	0.517	0.858
0.609	0.482	0.809	0.140	0.396	0.025	0.937	0.310	0.253	0.761
0.971	0.824	0.902	0.470	0.997	0.392	0.892	0.957	0.040	0.463
0.053	0.899	0.554	0.627	0.427	0.760	0.470	0.040	0.904	0.993
0.810	0.159	0.225	0.163	0.549	0.405	0.285	0.542	0.231	0.919
0.081	0.277	0.035	0.039	0.860	0.507	0.081	0.538	0.986	0.501
0.982	0.468	0.334	0.921	0.690	0.806	0.879	0.414	0.106	0.031
0.095	0.801	0.576	0.417	0.251	0.884	0.522	0.235	0.389	0.222
0.509	0.025	0.794	0.850	0.917	0.887	0.751	0.608	0.698	0.683
0.371	0.059	0.164	0.838	0.289	0.169	0.569	0.977	0.796	0.996
0.165	0.996	0.356	0.375	0.654	0.979	0.815	0.592	0.348	0.743
0.477	0.535	0.137	0.155	0.767	0.187	0.579	0.787	0.358	0.595
0.788	0.101	0.434	0.638	0.021	0.894	0.324	0.871	0.698	0.539
0.566	0.815	0.622	0.548	0.947	0.169	0.817	0.472	0.864	0.466
0.901	0.342	0.873	0.964	0.942	0.985	0.123	0.086	0.335	0.212
0.470	0.682	0.412	0.064	0.150	0.962	0.925	0.355	0.909	0.019
0.068	0.242	0.777	0.356	0.195	0.313	0.396	0.460	0.740	0.247
0.874	0.420	0.127	0.284	0.448	0.215	0.833	0.652	0.701	0.326
0.897	0.877	0.209	0.862	0.428	0.117	0.100	0.259	0.425	0.284
0.876	0.969	0.109	0.843	0.759	0.239	0.890	0.317	0.428	0.802
0.190	0.696	0.757	0.283	0.777	0.491	0.523	0.665	0.919	0.246
0.341	0.688	0.587	0.908	0.865	0.333	0.928	0.404	0.892	0.696
0.846	0.355	0.831	0.218	0.945	0.364	0.673	0.305	0.195	0.887
0.882	0.227	0.552	0.077	0.454	0.731	0.716	0.265	0.058	0.075
0.464	0.658	0.629	0.269	0.069	0.998	0.917	0.217	0.220	0.659
0.123	0.791	0.503	0.447	0.659	0.463	0.994	0.307	0.631	0.422
0.116	0.120	0.721	0.137	0.263	0.176	0.798	0.879	0.432	0.391
0.836	0.206	0.914	0.574	0.870	0.390	0.104	0.755	0.082	0.939
0.636	0.195	0.614	0.486	0.629	0.663	0.619	0.007	0.296	0.456
0.630	0.673	0.665	0.666	0.399	0.592	0.441	0.649	0.270	0.612
0.804	0.112	0.331	0.606	0.551	0.928	0.830	0.841	0.702	0.183
0.360	0.193	0.181	0.399	0.564	0.772	0.890	0.062	0.919	0.875
0.183	0.651	0.157	0.150	0.800	0.875	0.205	0.446	0.648	0.685

Figure 5-1. Random Numbers

DESIGN MIX FORMULA

The Producer is required to submit for the Engineer's approval a Design Mix Formula (DMF) for each mixture. This information is recorded in a format acceptable to the Engineer. TD-451 is one format that has been used for this purpose (Figure 5-2). INDOT is required to have a signed copy of the DMF prior to production of any mixture.

LOT/SUBLOT -- QC/QA HMA and SMA

Quality Assurance Specifications consider a lot as 4000 t of Base or Intermediate QC/QA HMA, and 2400 t of Surface QC/QA HMA or SMA. The lots are divided into four sublots of equal tons. For Base and Intermediate QC/QA HMA therefore, a sublot is 1000 t, and for Surface QC/QA HMA or SMA, a sublot is 600 t. Partial sublots of 100 t or less are added to the previous sublot. Partial sublots greater than 100 t constitute a full sublot.

ACCEPTANCE SAMPLES

Sampling of mixture for acceptance is made from the pavement in accordance with **ITM 580**. INDOT determines the random site and the Contractor obtains the samples under INDOT supervision.

A specific ton in each sublot is selected and the mixture from the truck containing that ton is sampled. This truck is determined by checking the weigh tickets. An example of how to determine what ton is to be sampled is indicated on form TD 452 (Figure 5-3). These random tons are not shown to the Contractor so that there is no possible influence on the construction operations.

Once the truck that contains the random ton is identified, the approximate total length of mixture that the truck places is determined by knowing the weight of the truck, the paving width, and the quantity placed. When placing variable depth, such as a crown correction, the average depth is used. The following relationship is used to calculate this approximate length that a truck would place.

Length of Load = Load Weight (t) x 18000
(Nearest Foot) Avg. Planned Quantity x Width of
$$(lb/yd^2)$$
 Paving (ft)

State Form XXXXX (R3/07-2002)

INDIANA DEPARTMENT OF TRANSPORTATION

CONTRACTOR T	Manda- O-	_1_		
	Wooden Const.			-21-02
	Wooden Cons	st.		-3000
	Lafayette		 	-65
PLANT NO.: 355 MIX DESIGN LAB: 014			-	rawfordsville
MIX DESIGN LAB: U14	19		REF. JMF:	t JMF No.
		MATERIA	AL SOURCES	
COARSE AGG. (SOURCE &	LEDGE):		FINE AGG.	(NAT./MAN. & SOURCE
2421 - Ledges 1-5,	18's		_2421 - Tedges 1-5	
2421 - Ledges 1-5,	11's			
PG BINDER (TYPE & SOUR	CE):		ANTI-STRIP A	GENT & DOSAGE RATE
PG 70-22, 7101	•		None Required	
	DESIGN N	MIX FORMU	ILA / JOB MIX FORMULA	
DMF/JMF number	0110133		Ignition oven test temp. °F	1000
Material code	3222	3		or 0.42
ESAL	15,000,0		Ignition oven serial number	21
Mixture type	19.0 mm		Binder % actual (ig. ov.)	21 4.5
	19.0 mm 1 in.	Int.		
Mixture type Maximum particle size	19.0 mm 1 in.		Binder % actual (ig. ov.) Binder % extracted	4.5
Mixture type Maximum particle size % Pass 1 1/2 in.	19.0 mm 1 in. MASS	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No	4.5
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in.	19.0 mm 1 in. MASS \	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax	4.5
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in.	19.0 mm 1 in. MASS \ 100 95.3	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes	4.5 4.3 No 8/100/100 151.6
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in.	19.0 mm 1 in. MASS \	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma	4.5 4.3 No 8/100/100 151.6 ax 2.480
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 3/8 in.	19.0 mm 1 in. MASS \ 100 95.3	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate)	4.5 4.3 No 8/100/100 151.6
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 3/8 in. % Pass No. 4	19.0 mm 1 in. MASS 100 95.3 81.0	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes	4.5 4.3 No 8/100/100 151.6 ax 2.480
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 3/8 in. % Pass No. 4 % Pass No. 8	19.0 mm 1 in. MASS \ 100 95.3 81.0 25.0	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 3/8 in. % Pass No. 4 % Pass No. 8 % Pass No. 30	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes	4.5 4.3 No 8/100/100 151.6 ex 2.480 2.538 4.3
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 3/8 in. % Pass No. 4 % Pass No. 8	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5 4.2	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes VFA @ Ndes Coarse aggregate angularity	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538 4.3 13.5 68.1
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 1/2 in. % Pass No. 4 % Pass No. 4 % Pass No. 8 % Pass No. 30 % Pass No. 200 Gsb	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes VFA @ Ndes	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538 4.3 13.5 68.1
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 3/8 in. % Pass No. 4 % Pass No. 8 % Pass No. 30 % Pass No. 200 Gsb Mix temperature min. °F	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5 4.2 2.682 260	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes VFA @ Ndes Coarse aggregate angularity	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538 4.3 13.5 68.1
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 1/2 in. % Pass No. 4 % Pass No. 4 % Pass No. 8 % Pass No. 30 % Pass No. 200 Gsb	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5 4.2 2.682	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes VFA @ Ndes Coarse aggregate angularity	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538 4.3 13.5 68.1
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 3/8 in. % Pass No. 4 % Pass No. 8 % Pass No. 30 % Pass No. 200 Gsb Mix temperature min. °F	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5 4.2 2.682 260	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes VFA @ Ndes Coarse aggregate angularity Fine aggregate angularity Sand equivalency	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538 4.3 13.5 68.1
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 1/2 in. % Pass No. 4 % Pass No. 4 % Pass No. 8 % Pass No. 30 % Pass No. 200 Gsb Mix temperature min. °F Mix temperature max °F	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5 4.2 2.682 260 325	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes VFA @ Ndes Coarse aggregate angularity Fine aggregate angularity Sand equivalency Dust/calculated effective bin	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538 4.3 13.5 68.1 48.0 85.0 der 1.00
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 1/2 in. % Pass 3/8 in. % Pass No. 4 % Pass No. 8 % Pass No. 30 % Pass No. 200 Gsb Mix temperature min. °F Mix temperature max °F RAP % in mixture RAP binder % extracted	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5 4.2 2.682 260 325 0	Int.	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes VFA @ Ndes Coarse aggregate angularity Fine aggregate angularity Sand equivalency Dust/calculated effective bin Tensile strength ratio	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538 4.3 13.5 68.1 48.0 85.0 der 1.00 86.9
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 1/2 in. % Pass 3/8 in. % Pass No. 4 % Pass No. 8 % Pass No. 30 % Pass No. 200 Gsb Mix temperature min. °F Mix temperature max °F RAP % in mixture	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5 4.2 2.682 260 325 0	VOLUME	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes VFA @ Ndes Coarse aggregate angularity Fine aggregate angularity Sand equivalency Dust/calculated effective bin Tensile strength ratio	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538 4.3 13.5 68.1 48.0 85.0 der 1.00
Mixture type Maximum particle size % Pass 1 1/2 in. % Pass 1 in. % Pass 3/4 in. % Pass 1/2 in. % Pass 1/2 in. % Pass 3/8 in. % Pass No. 4 % Pass No. 8 % Pass No. 30 % Pass No. 200 Gsb Mix temperature min. °F Mix temperature max °F RAP % in mixture RAP binder % extracted	19.0 mm 1 in. MASS 100 95.3 81.0 25.0 10.5 4.2 2.682 260 325 0	VOLUME	Binder % actual (ig. ov.) Binder % extracted MSG w/ dry back Yes or No Gyrations Nini/Ndes/Nmax Density, kg/m³ @ Ndes Gmb (plot/calculate) @ Nma Gmm (plot/calculate) % Air voids @ Ndes VMA @ Ndes VFA @ Ndes Coarse aggregate angularity Fine aggregate angularity Sand equivalency Dust/calculated effective bin Tensile strength ratio	4.5 4.3 No 8/100/100 151.6 ax 2.480 2.538 4.3 13.5 68.1 48.0 85.0 der 1.00 86.9

Figure 5-2. Design Mix Formula

·					ĺ	ī		1				1.		1		
			10/01/	RANDOM STATION	- -	N.B. Passing	10+85	N.P. Passing	77+33	N.B. Passing	194+90	N.B.	247+75			
			SUBLOT 4 6/10/01	STARTING STA.*	-		10+50		76+90		194+00	•	247+20			
		diate	10	RANDOM DIST.	G × H = 1		35		43		90		55			
7		19.0 mm Intermediate	SUBLOT 3 6/10/01	RANDOM NO.	I		.259	·	.317		.665		.404			
INDIANA DEPARTMENT OF TRANSPORTATION DIVISION OF MATERIALS AND TESTS RANDOM SAMPLING FOR MIX ANALYSIS	4	19.0 ш	.O.BLO.	LENCTH OF LOAD	U		136		136		136		136			
DIANA DEPARTMENT OF TRANSPORTATION DIVISION OF MATERIALS AND TESTS RANDOM SAMPLING FOR MIX ANALYSIS	è S	e e	10/	TRANS. LOC.	m ×		$\begin{array}{c} 1.2 \\ (1) \end{array}$		10.7 (11)		6.3 (6)		(11)	ADING.	× 18000	
MENT OF MATERIA PLING FO	LOT No.	Mixture	SUBLOT 2 6/9/01	RANDOM NO.	u.		.100		.890		.523		.928	SINS UNIC	Width of Paving (ft.)	
SION OF			SUBL	PAVING WIDTH	W		12		12		12		12	1 TON BEC	ght (tons) ntity × V	
INDIANA DIV RAND			10/6/	r TON SAMPLED	C + D		123		1116		2836		3636	RANDON	Load Weight (tons) Planned Quantity × 1. yd.)	
	وب	ield	SUBLOT 1 6	10 BE	۵	0	0	625	1000	1250	2000	1875	3000	NTAINING	Avg. Plann (lb./sq. yd.)	
æ	R-20396	Greenfield		RANDOM	A × B = C		123		116		836		636	TRUCK CO	Load = 'oot)	
Slate Form 36667 (R3/3-95) : ESTING ENGINEER	Contract No	District	DATE SAMPLED:	RANDOM NO.	6		.123		.116		.836	•	.636	ER WHEN	Length of Load (Nearest Foot)	
TD-452 State Form 36667 (R COPIES TO: DISTRICT TESTING ENGINEER FILE	Con	Dist	DAT	SUBLOT TONS	<	009	1000	900	1000	900	1000	009	1000	STATION OF PAVER WHEN TRUCK CONTAINING RANDOM TON BEGINS UNLOADING.		
TD-452 S COPIES TO: DISTRICT TE				SUBLOT		*		~		~	,	-4	,	• STATIO!		

Figure 5-3. Random Sampling for Mix

The length the truck places is multiplied by the first random number to obtain a longitudinal distance. This distance is measured from the location of the paver when the truck containing the random ton begins unloading into the paver or material transfer device. The transverse test site location is determined by multiplying the width of pavement by the second random number and rounding to the nearest whole ft. This distance is measured from the right edge of pavement when looking in the direction of increasing station numbers. If the transverse location is less than 1 ft from either edge of pavement, at a location where the course thickness is less than 2.0 times the maximum particle size, or within the width of the roller drum used to form shoulder corrugations, then another random location is selected to obtain an acceptable sampling location. The following example indicates how these random locations are determined.

Example

Width of Pavement = 12 ft Load Weight = 20 t

Mixture = 9.5 mm Surface

Planned Quantity = 110 lb/yd^2

Ending Station of Paver

of Previous Load = 158+00 Random Numbers = 256, .561

Test Site Station

Length of Load
$$= \frac{20}{110 \times 12}$$
 x $18000 = 273$ ft

Longitudinal Distance =
$$273 \times .256 = 70 \text{ ft}$$

Random Station
$$= (158+00) + 70 = 158+70$$

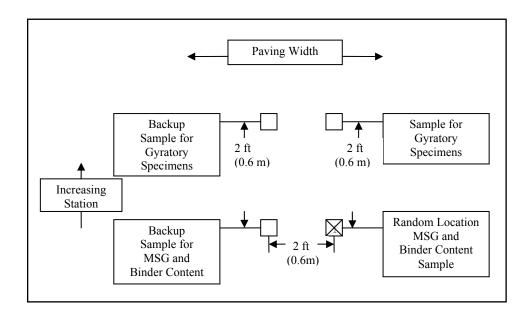
Transverse Distance

Distance =
$$12 \times .561 = 6.7 \text{ ft (say 7 ft)}$$

For contracts controlled by volumetrics for QC/QA HMA (401), several samples are required. The first plate sample location is determined by the random sampling procedure and this material is used for the maximum specific gravity and binder content samples. A second plate sample is placed longitudinally 2 ft upstation from the first plate at the same transverse offset. This sample is used for the gyratory specimens.

If an appeal by the Producer of the INDOT test results is accepted, backup samples are tested. These samples are obtained at the same time as the acceptance samples. The backup sample plate for the maximum specific gravity and binder content is placed transversely 2 ft from the first plate towards the center of the mat. The backup sample for the gyratory specimens is placed transversely 2 ft from the second plate towards the center of the mat.

The following diagram indicates an example of an arrangement of the plate samples when additional samples are required for QC/QA HMA:



An example of determining the sample locations is as follows:

Width of Pavement = 12 ftLoad Weight = 20 t

Mixture = 9.5 mm SurfacePlanned Quantity = 110 lb/yd^2

Ending Station of Paver

of Previous Load = 158+00 Random Numbers = . 256, .561

Test Site Station

Length of Load
$$= \frac{20}{110 \times 12}$$
 x $18000 = 273$ ft

Longitudinal Distance = $273 \times .256 = 70 \text{ ft}$

Random Station
$$= (158+00) + 70 = 158+70$$

Transverse Distance

Distance =
$$12 \times .561 = 6.7 \text{ ft (say 7 ft)}$$

MSG and Binder Content Sample

Random Location = 158 + 70

Transverse Distance = 7 ft

Gyratory Specimens Sample

Random Location =
$$(158 + 70) + 02$$

= $158 + 72$

Transverse Location = 7 ft

Backup Sample for MSG and Binder Content

Random Location = 158 + 70

Transverse Distance = 7-2

= 5 ft

Backup Sample for Gyratory Specimens

Random Location
$$= (158 + 70) + 2$$

= 158 + 72

Transverse Distance = 7-2

= 5 ft

The size of the plate used to obtain a sample is dependent on the test (s) conducted on the material. The following minimum sample weights are required:

Mixture	Minimum Weights (g)				
Designation	MSG and Binder	Gyratory			
Designation	Content	Specimens			
4.75 mm	1200	11000			
9.5 mm	3000	11000			
12.5 mm	4000	11000			
19.0 mm, OG 19.0 mm	5500	11000			
25.0 mm, OG 25.0 mm	7000	11000			

Figure 5-4 indicates the approximate weights that may be obtained for various sizes of plates and lift thicknesses that are placed.

Figure 5-5 indicates the approximate weights that may be obtained for various sizes of molds and lift thicknesses when a mold is used with the plate for obtaining a sample.

ADJUSTMENT PERIOD -- QC/QA HMA and SMA

The Producer is allowed an adjustment period for each mix design in which the mix design is verified and changes may be made in the DMF, if necessary. A job mix formula (JMF) is submitted for approval to the Engineer upon completion of the adjustment period. The adjustment period is from the beginning of production and extending until 4000 t of base or intermediate QC/QA HMA, or 2400 t of surface QC/QA HMA or SMA has been produced for each mix design. A reduced adjustment period is allowed. If production extends into the next construction season, another adjustment period is allowed.

	Approximate Sample Yield for Various Lift Thickness and Plate Sizes							
Lift	Lay			Pla	te Size, inc	hes		
Thickness (inches)	Rate (lb/syd)	8	9	10	11	12	14	16
			•	San	nple Weigh	t (g)	•	
1.25	137.5	3100	3900	4800	5900	7000	9500	12400
1.5	165	3700	4700	5800	7000	8400	11400	14900
1.75	192.5	4300	5500	6800	8200	9800	13300	17300
2.0	220	5000	6300	7700	9400	11100	15200	19800
2.25	247.5	5600	7100	8700	10500	12500	17100	22300
2.5	275	6200	7800	9700	11700	13900	19000	27800
2.75	302.5	6800	8600	10600	12900	15300	20900	27300
3.0	330	7400	9400	11600	14100	16700	22800	29700
3.25	357.5	8100	10200	12600	15200	18100	24700	32200
3.5	385	8700	11000	13500	16400	19500	26600	34700
3.75	412.5	9300	11800	14500	17600	20900	28500	37200
4.0	440	9900	12500	15500	18700	22300	30300	39600
4.25	467.5	10500	13300	16400	19800	23600	32100	41900
4.5	495	11100	14000	17300	21000	25000	34000	44400
4.75	522.5	11700	14800	18300	22100	26400	35900	46900
5.0	550	12300	15600	19300	23300	27700	37800	49300
5.25	577.5	12900	16400	20200	24500	29100	39700	51800
5.5	605	13600	17200	21200	25600	30500	41500	54300
5.75	632.5	14200	17900	22200	26800	31900	43400	56700
6.0	660	14800	18700	23100	28000	33300	45300	59200

Figure 5-4. Approximate Sample Yield for Various Lift Thickness and Plate Sizes

Approximate Sample Yield for Various Lift Thicknesses and Mold Sizes						
Lift	Lay Rate			old Size, incl		
Thickness (inches)	(lb/yd²)	8	10	12	14	16
			Sai	mple Weight	(g)	
1.25	137.5	2400	3800	5400	7400	9700
1.5	165	2900	4500	6500	8900	11600
1.75	192.5	3400	5300	7600	10400	13600
2.0	220	3900	6100	8700	11900	15500
2.25	247.5	4400	6800	9800	13300	17400
2.5	275	4800	7600	10900	14800	19400
2.75	302.5	5300	8300	12000	16300	21300
3.0	330	5800	9100	13100	17800	23200
3.25	357.5	6300	9800	14200	19300	25200
3.5	385	6800	10600	15300	20800	27100
3.75	412.5	7300	11300	16300	22200	29100
4.0	440	7700	12100	17400	23700	31000
4.25	467.5	8200	12900	18500	25200	32900
4.5	495	8700	13600	19600	26700	34900
4.75	522.5	9200	14400	20700	28200	36800
5.0	550	9700	15100	21800	29700	38700
5.25	577.5	10200	15900	22900	31100	40700
5.5	605	10700	16600	24000	32600	42600
5.75	632.5	11100	17400	25100	34100	44500
6.0	660	11600	18200	26100	35600	46500

Figure 5-5. Approximate Sample Yield for Various Lift Thicknesses and Mold Sizes

MIXTURE ACCEPTANCE

QC/QA HMA

Acceptance of QC/QA HMA mixtures for binder content, VMA at N_{des} , and air voids at N_{des} for each lot is based on tests conducted by INDOT. INDOT randomly select the location(s) within each sublot for sampling in accordance with the **ITM 802.**

Samples from the pavement are obtained from each sublot in accordance with **ITM 580**. The test results for each sublot are required to be within the tolerances from the JMF as shown in the table as follows:

ACCEPTANCE TOLERANCES						
MIXTURE PROPERTIES	TOLERANCES FROM JMF					
DENSE GRADED						
Air Voids	$JMF \pm 1.0\%$					
Binder Content	$JMF \pm 0.5\%$					
VMA	$JMF \pm 1.0\%$					
OPEN (OPEN GRADED					
Air Voids *	JMF ± 3.0%					
Binder Content	$JMF \pm 0.5\%$					

^{*} Gmb is determined in accordance with **ASTM D 6752**

A binder draindown test in accordance with **AASHTO T 305** for open graded mixtures is required once per lot and may exceed 0.50 %.

The acceptance test results for each sublot are available after the sublot and the testing are complete.

HMA

Acceptance of HMA mixtures is done on the basis of a Type D certification submitted by the Producer to the Project Engineer on a contract. An example of this form is shown in Figure 5-6. The certification is required to be submitted with the first truck of each type of mixture each day. If no test results are available, the Producer indicates on the form that test results are required to be obtained within the first 250 tons and each subsequent 1000 tons for base and intermediate mixtures, and the first 250 tons and each subsequent 600 tons for surface mixtures.

INDIANA DEPARTMENT OF TRANSPORTATION HOT MIX ASPHALT (HMA) CERTIFICATION

CONTRACT NUMBER RS-30000 DATE 5/3/05
CERTIFIED HMA PRODUCER J. Wooden Construction
CERTIFIED HMA PLANT NUMBER 3550
DMF/ JMF NUMBER0310075
MIXTURE TYPE AND SIZE HMA Surface, 9.5 mm, Type A
DESIGN ESAL 200,000
Air Voids (from DMF/JMF) Binder Content (from DMF/JMF)
This is to certify that the following test results for Air Voids and Binder Content represent the HMA mixture supplied to this contract:
Air Voids 4.3 (± 1.5 % from DMF/JMF) Binder Content 5.7 (± 0.7 % from DMF/JMF)
*[] Test results are not available for submittal. A production sample shall be taken within the first 250 t (250 Mg), and each subsequent 1000 t (1000 Mg) for base and intermediate mixtures and each subsequent 600 t (600 Mg) for surface mixtures.
* If Applicable
Signature of HMA Producer Official
Title of Official
FOR PE/PS USE ONLY
PAY ITEM(S) BASIS FOR USE NO. <u>C999998</u>
SPECIFICATION REFERENCE 402.07(c) - Temporary HMA 610.03 - Approaches 304.04 - Patching 503.03(e) - Terminal Joints 610.03 - Crossovers 402 HMA Pavements 507.05(b) - Partial Depth Patch 718.02 - Underdrains 402.07(a) - Rumble Strips 604.07(c) - Sidewalk 801.11 - Temp.Cross. 402.07(b) - Wedge & Leveling 605.07(c) - Curbing

Figure 5-6. HMA Certification

SMA

Acceptance of SMA mixtures for binder content and gradation for each sublot is based on tests conducted by INDOT. The sample locations are determined by INDOT in accordance with **ITM 802** and samples are obtained from each sublot in accordance with **ITM 580**.

Test results for binder content, and gradation may not exceed the allowable tolerances of Section **401.09**. A binder draindown test in accordance with **AASHTO T 305** is required once per lot and may not exceed 0.30 %. The acceptance test results for each sublot are available after the sublot and the testing are complete.

PAY FACTORS -- QC/QA HMA

After the tests are conducted, the test data is evaluated for compliance with the Specifications. CAA and temperature tests are taken in accordance with standard procedures and recorded. Lot numbers begin with number 1 for each type of mixture and are continuous for the entire contract regardless of the number of adjustment periods for that type of mixture.

When the required tests for one sublot are completed, the difference between the test values and the required value on the JMF is determined and pay factors calculated. For mixtures produced during the adjustment period, pay factors based on the JMF are used. A composite pay factor for each sublot is determined for the binder content, air voids @ N_{des} , VMA @ N_{des} , and density of the mixture as follows:

$$SCPF = 0.20(PF_{BINDER}) + 0.35(PF_{VOIDS}) + 0.10(PF_{VMA}) + 0.35(PF_{DENSITY})$$

where.

SCPF = Sublot Composite Pay Factor for Mixture and Density

PF_{BINDER} = Sublot Pay Factor for Binder Content

PF_{VOIDS} = Sublot Pay Factor for Air Voids at N_{des}

PF_{VMA} = Sublot Pay Factor for VMA at N_{des}

PF_{DENSITY} = Sublot Pay Factor for Density

If the SCPF for a sublot is less than 0.85, the pavement is evaluated by INDOT. If the Contractor is not required to remove the mixture, quality assurance adjustments of the sublot are assessed or other corrective actions taken as determined by INDOT.

MIXTURE

Sublot test results for mixture properties are assigned pay factors in accordance with the following:

BINDER CONTENT					
DENSE GRADED Deviation from JMF	OPEN GRADED Deviation from JMF	PAY FACTOR			
(±%)	(±%)				
≤ 0.2	≤ 0.2	1.05			
0.3	0.3	1.04			
0.4	0.4	1.02			
0.5	0.5	1.00			
0.6	0.6	0.90			
0.7	0.7	0.80			
0.8	0.8	0.60			
0.9	0.9	0.30			
1.0	1.0	0.00			
> 1.0	> 1.0	Submit to the			
		Office of Materials			
		Management*			

^{*} Test results are considered and adjudicated as a failed material in accordance with normal INDOT practice as listed in 105.03.

AIR VOIDS					
DENSE GRADED Deviation from JMF (±%)	OPEN GRADED Deviation from JMF (±%)	PAY FACTOR			
≤ 0.5	≤ 1.0	1.05			
$> 0.5 \text{ and } \le 1.0$	$> 1.0 \text{ and } \le 3.0$	1.00			
1.1	3.1	0.98			
1.2	3.2	0.96			
1.3	3.3	0.94			
1.4	3.4	0.92			
1.5	3.5	0.90			
1.6	3.6	0.84			
1.7	3.7	0.78			
1.8	3.8	0.72			
1.9	3.9	0.66			
2.0	4.0	0.60			
> 2.0	> 4.0	Submit to the Office of Materials			
		Management			

^{*} Test results are considered and adjudicated as a failed material in accordance with normal INDOT practice as listed in 105.03.

VMA					
DENSE GRADED Deviation from JMF	OPEN GRADED Deviation from JMF	PAY FACTOR			
(±%)	$(\pm \%)$				
≤ 0.5		1.05			
$> 0.5 \text{ and} \le 1.0$	All	1.00			
$> 1.0 \text{ and } \le 1.5$		0.90			
$> 1.5 \text{ and } \le 2.0$		0.70			
$> 2.0 \text{ and } \le 2.5$		0.30			
> 2.5		Submit to the			
		Office of Materoals			
		Management*			

^{*} Test results are considered and adjudicated as a failed material in accordance with normal INDOT practice as listed in 105.03.

DENSITY

Sublot test results for density are assigned pay factors in accordance with the following:

	DENSITY				
Percentages based on % MSG	Pay Factors – Percent				
Dense Graded	Open Graded				
≥ 97.0		Submitted to the Office of Materials Management*			
95.6 - 96.9		1.05 - 0.01 for each 0.1% above 95.5			
94.0 - 95.5		1.05			
93.1 - 93.9		1.00 + 0.005 for each 0.1% above 93.0			
92.0 - 93.0	84.0	1.00			
91.0 - 91.9		1.00 - 0.005 for each 0.1% below 92.0			
90.0 - 90.9		0.95 - 0.010 for each 0.1% below 91.0			
89.0 - 89.9		0.85 - 0.030 for each 0.1% below 90.0			
≤ 88.9		Submitted to the Office of Materials Management*			

^{*} Test results are considered and adjudicated as a failed material in accordance with normal INDOT practice as listed in 105.03.

Figure 5-7 indicates the density pay factors required for the % Maximum Specific Gravity of the cores.

DENSITY DENSE GRADED									
% MSG	Pay Factor	% MSG	Pay Factor	% MSG	Pay Factor	% MSG	Pay Factor		
≥97.0	*	94.9	1.05	92.8	1.00	90.7	0.92		
96.9	0.91	94.8	1.05	92.7	1.00	90.6	0.91		
96.8	0.92	94.7	1.05	92.6	1.00	90.5	0.90		
96.7	0.93	94.6	1.05	92.5	1.00	90.4	0.89		
96.6	0.94	94.5	1.05	92.4	1.00	90.3	0.88		
96.5	0.95	94.4	1.05	92.3	1.00	90.2	0.87		
96.4	0.96	94.3	1.05	92.2	1.00	90.1	0.86		
96.3	0.97	94.2	1.05	92.1	1.00	90.0	0.85		
96.2	0.98	94.1	1.05	92.0	1.00	89.9	0.82		
96.1	0.99	94.0	1.05	91.9	1.00	89.8	0.79		
96.0	1.00	93.9	1.05	91.8	0.99	89.7	0.76		
95.9	1.01	93.8	1.04	91.7	0.99	89.6	0.73		
95.8	1.02	93.7	1.04	91.6	0.98	89.5	0.70		
95.7	1.03	93.6	1.03	91.5	0.98	89.4	0.67		
95.6	1.04	93.5	1.03	91.4	0.97	89.3	0.64		
95.5	1.05	93.4	1.02	91.3	0.97	89.2	0.61		
95.4	1.05	93.3	1.02	91.2	0.96	89.1	0.58		
95.3	1.05	93.2	1.01	91.1	0.96	89.0	0.55		
95.2	1.05	93.1	1.01	91.0	0.95	88.9	*		
95.1	1.05	93.0	1.00	90.9	0.94				
95.0	1.05	92.9	1.00	90.8	0.93				
	DENSITY OPEN GRADED								
84.0 1.00									

* Requires submittal to Office of Materials Management for Failed Material Investigation

Figure 5-7. Density Pay Factors

The following example indicates how Quality Assurance Adjustments are determined:

Example

25.0 mm Base

Sublot 1 = 1000 tons Sublot 2 = 1000 tons

Sublot 3 = 1000 tons

Sublot 4 = 1000 tons

Unit Price = \$28.00/ton

MAF = 1.000

JMF % Binder = 4.2 %

Air Voids = 4.0 %

VMA = 12.5 %

	Sublot 1	Sublot 2	Sublot 3	Sublot 4
% Binder	4.5	4.6	4.8	4.2
Air Voids	3.8	3.7	3.2	4.7
VMA	12.2	12.1	11.6	13.4
Density (%MSG)	91.1	90.7	89.9	92.9

Deviations for JMF % Binder, Air Voids, and VMA:

	Sublot 1	Sublot 2	Sublot 3	Sublot 4
% Binder	0.3	0.4	0.6	0.2
Air Voids	0.2	0.3	0.8	0.7
VMA	0.3	0.4	0.9	0.9

Using the pay factor charts, the following values are obtained:

	Sublot 1	Sublot 2	Sublot 3	Sublot 4
% Binder	1.04	1.02	0.90	1.05
Air Voids	1.05	1.05	1.00	1.00
VMA	1.05	1.05	1.00	1.00
Density (%MSG)	0.96	0.92	0.82	1.00

Calculations to determine the Quality Assurance Adjustment are indicated in Figure 5-8.

INDIANA DEPARTMENT OF TRANSPORTATION HOT MIX ASPHALT ANALYSIS FOR QUALITY ASSURANCE

CONTRACT NO	PLANT NO	LOT NO	DATE	
MIXTURE		DMF/JMF	NO.	

Mixture &	SUBLOT 1		S	UBLO	Γ2	SUBLOT 3		3 SUBLOT		7 4		
Density	Pay Factor	Mult		Pay Factor	Mult		Pay Factor	Mult.		Pay Factor	Mult.	
%												
Binder	1.04	0.20	0.2080	1.02	0.20	0.2040	0.90	0.20	0.1800	1.05	0.20	0.2100
Air												
Voids	1.05	0.35	0.3675	1.05	0.35	0.3675	1.00	0.35	0.3500	1.00	0.35	0.3500
VMA	1.05	0.10	0.1050	1.05	0.10	0.1050	1.00	0.10	0.1000	1.00	0.10	0.1000
Density	0.96	0.35	0.3360	0.92	0.35	0.3220	0.82	0.35	0.2870	1.00	0.35	0.3500
SCPF			1.02			1.00			0.92			1.01

^{*} Requires submittal to the Materials and Tests Division for Failed Material Investigation

QUALITY ASSURANCE ADJUSTMENTS									
Sublot 1 Quantity L (tons)	Sublot 1 Adjustment (\$)	Sublot 2 Quantity L (tons)	Sublot 2 Adjustment (\$)	Sublot 3 Quantity L (tons)	Sublot 3 Adjustment (\$)	Sublot 4 Quantity L (tons)	Sublot 4 Adjustment (\$)		
1000	+560	1000	0	1000	-2240	1000	+280		

U = Unit Price for Material, \$/Ton

Quality Assurance Adjustment = L x U x (SCPF – 1.00) / MAF

Figure 5-8. Quality Assurance Adjustment

MIX APPEAL -- QC/QA HMA

If the Producer does not agree with the acceptance test results, a request may be submitted in writing that additional samples be tested. The written request is required to include the Producer's test results and be made within seven calendar days of receipt of the written results of the HMA tests for that lot. The appeal is not accepted if the Producer has not conducted any tests that indicate a higher Pay Factor than was determined from the test results by INDOT.

Additional tests for the appeal may be requested for the maximum specific gravity, bulk specific gravity of the gyratory specimens, binder content, or bulk specific gravity of the density cores. One or more of these tests may be requested for the sublot or entire lot. Upon approval of the appeal, the backup samples are tested as follows:

- 1) Maximum Specific Gravity -- The sample is dried in accordance with **ITM 572** and tested in accordance with **AASHTO T 209**, Section 9.5.1.
- 2) Bulk Specific Gravity of the Gyratory Specimens -- New gyratory specimens are prepared and tested in accordance with **AASHTO T 312**.
- 3) Binder Content -- The binder content is tested in accordance with the test method that was used for acceptance.
- 4) Bulk Specific Gravity of the Density Core -- Additional cores are taken within seven calendar days unless otherwise directed. The core locations are determined by adding 1.0 ft longitudinally of the cores tested for acceptance using the same transverse offset. The cores are tested in accordance with **AASHTO T 166**.

The appeal results replace all previous test result(s) for acceptance of the mixture properties and density.

ADJUSTMENT QUANTITY -- QC/QA HMA

The pay factors are used to calculate a quality assurance adjustment quantity (q) for the sublot. The adjustment for mixture properties and density is calculated as follows:

$$q = L \times U \times (SCPF - 1.00)/MAF$$

where:

q = quality assurance adjustment for the sublot

L = sublot quantity

U = unit price for the material, \$/Ton

SCPF = sublot composite pay factor

The total quality assurance adjustments are calculated as follows:

$$Q = Q_S + (\Sigma q)$$

where:

Q = total quality assurance adjustment

Qs = quality assurance adjustment for smoothness as calculated in Section **401.19(c)**

q = sublot quality assurance adjustment

ADJUSTMENT QUANTITY - SMA

The adjustment points are used to calculate a quality assurance adjustment quantity (q) for the sublot. The adjustment for mixture properties and density is calculated as follows:

$$q = (L \times U \times P/100)/MAF$$

where:

q = quality assurance adjustment quantity

L = lot quantity

U = unit price for material, \$/TON

P = total adjustment points

The total quality assurance adjustments are to be calculated as follows:

$$Q = Q_s + 3 (q_m + q_d)$$

where:

Q = total quality assurance adjustment quantity

 Q_s = quality assurance adjustment for smoothness as calculated in Section **401.19(c)**

 $q_m = lot adjustments for mixtures$

 $q_d = lot adjustments for density$

MIXTURE ADJUSTMENT FACTOR

A Mixture Adjustment Factor (MAF) is used to adjust the mixture planned quantity and lay rate prior to paving operations, and the pay quantity upon completion of production of the mixture. The MAF is calculated by dividing the maximum specific gravity (G_{mm}) from the mixture design by the following values:

<u>Mixture</u>
9.5 mm -- 2.465
12.5 mm -- 2.500
19.0 mm -- 2.500
25.0 mm -- 2.500

If the calculated MAF is equal to or greater than 0.980 and equal to or less than 1.020, then the MAF value is considered to be 1.000. If the calculated MAF is less than 0.980 or greater than 1.020 then the MAF is the actual calculated value. The planned quantity and lay rate are adjusted by multiplying by the MAF. The accepted quantity for payment is adjusted by dividing by the MAF.

Example

Mixture 9.5 mm Surface Planned Quantity 9750.00 tons Placed Quantity 9500.00 tons = Mix Design G_{mm} 2.360 165 lb/yd^2 Lay Rate MAF = 2.360 = 0.9572.465 Adjusted Planned Quantity = $0.957 \times 9750.00 = 9330.75 \text{ tons}$ Adjusted Lav Rate = $0.957 \times 165 \text{ lb/yd}^2 = 158 \text{ lb/yd}^2$ Adjusted Pay Quantity = 9500.00 = 9926.85 tons

0.957

The MAF does not apply to open graded mixtures.